



# **ProcessSCAN**

#### Infrared Thermographic Services













# **RTOS** (Recuperative Thermal Oxidizers)

![](_page_4_Picture_1.jpeg)

# RTOS (Recuperative Thermal Oxidizers)

![](_page_5_Picture_1.jpeg)

![](_page_6_Picture_0.jpeg)

![](_page_6_Picture_1.jpeg)

![](_page_6_Picture_2.jpeg)

![](_page_6_Picture_3.jpeg)

![](_page_6_Picture_4.jpeg)

![](_page_7_Figure_0.jpeg)

![](_page_7_Picture_1.jpeg)

![](_page_7_Picture_2.jpeg)

Heating process monitoring

![](_page_7_Picture_4.jpeg)

![](_page_8_Figure_0.jpeg)

### Fluid Machine Analysis

![](_page_9_Picture_1.jpeg)

![](_page_10_Picture_0.jpeg)

## Dry Chemical Pumping Systems

![](_page_10_Picture_2.jpeg)

![](_page_10_Picture_3.jpeg)

![](_page_11_Figure_0.jpeg)

📾 Start 🛛 🙆 😂 🖸 🕨 🗷 🐼 🖓 🖾 🖼 🕅 🖾 🖉 🌢 🍪 🎸 🍃 🗱 🗀 🌩

![](_page_12_Figure_0.jpeg)

# BLOWERS

![](_page_13_Figure_1.jpeg)

![](_page_13_Picture_2.jpeg)

# BLOWERS

![](_page_14_Figure_1.jpeg)

![](_page_14_Picture_2.jpeg)

# BLOWERS

![](_page_15_Figure_1.jpeg)

![](_page_15_Picture_2.jpeg)

![](_page_16_Picture_0.jpeg)

### Infrared

Surveying

for

Machine Evaluation

![](_page_16_Picture_5.jpeg)

![](_page_17_Picture_0.jpeg)

#### Warmest Spot: 202.7

#### Coolest Spot: 151.0

![](_page_17_Picture_3.jpeg)

![](_page_17_Picture_4.jpeg)

![](_page_18_Picture_0.jpeg)

![](_page_18_Picture_1.jpeg)

# Infrared Surveying for Machine **Evaluation**

![](_page_18_Picture_3.jpeg)

![](_page_19_Picture_0.jpeg)

![](_page_19_Picture_1.jpeg)

Infrared Surveying for Machine **Evaluation** 

![](_page_19_Picture_3.jpeg)

## IR Surveying of Freezers/Coolers and Blast Chillers

![](_page_20_Picture_1.jpeg)

## IR Surveying of Freezers/Coolers and Blast Chillers

![](_page_21_Figure_1.jpeg)

![](_page_21_Figure_2.jpeg)

#### Leak in Drain Lines

22

20

18

16

![](_page_21_Picture_4.jpeg)

IR Surveying of Freezers/Coolers and Blast Chillers

![](_page_22_Picture_1.jpeg)

## Spinnerettes (extrusion dies) for textiles

![](_page_23_Picture_1.jpeg)

![](_page_23_Picture_2.jpeg)

![](_page_24_Picture_0.jpeg)

![](_page_24_Picture_1.jpeg)

# Motor Rotor Testing

![](_page_24_Picture_3.jpeg)

![](_page_25_Picture_0.jpeg)

### Area 2 Max 31.4 Delta -T = 5.5 C degrees Area 1 Min 25.9

# Motor Stator Testing

![](_page_25_Picture_3.jpeg)

![](_page_26_Picture_0.jpeg)

![](_page_26_Picture_1.jpeg)

### FINDING CONDENSATE RETURN LINE LEAKS

ProcessSCAN Infrared Thermographic Services

### Aerostat Helium Leakage Detection using Infrared Thermography

ProcessSCAN's technique relies on detecting very small temperature differences to see the escape of helium (or other gases). The gas itself is not visible, but the cooling effect of escaping gas impinging on the surface is detected. We methodically go down the surfaces quickly and close enough to see the small, cooler areas.

![](_page_27_Picture_2.jpeg)

![](_page_27_Figure_3.jpeg)

![](_page_28_Picture_0.jpeg)

![](_page_28_Picture_1.jpeg)

![](_page_28_Figure_2.jpeg)

Histogram AR01

![](_page_28_Figure_3.jpeg)

![](_page_28_Figure_4.jpeg)

## Cartridge Heating Plate

WYPALL X60

156

ProcessSCAN

![](_page_30_Picture_0.jpeg)

![](_page_30_Picture_1.jpeg)

![](_page_30_Picture_2.jpeg)

![](_page_31_Figure_0.jpeg)

## **Machine Monitoring**

![](_page_32_Figure_1.jpeg)

![](_page_32_Figure_2.jpeg)

## **Machine Monitoring**

![](_page_33_Figure_1.jpeg)

![](_page_33_Figure_2.jpeg)

# Quantifying air leakage in pressurization chambers

![](_page_34_Picture_1.jpeg)

![](_page_34_Picture_2.jpeg)

#### Air in-leakage at com outlet

![](_page_34_Picture_4.jpeg)

#### Computer Room Analysis

![](_page_35_Picture_1.jpeg)

G1 BCDEFGH (

- 153

- 18

![](_page_36_Picture_0.jpeg)

Infrared Thermographic Services

#### Computer Room Analysis

![](_page_36_Picture_3.jpeg)

![](_page_36_Picture_4.jpeg)

![](_page_36_Picture_5.jpeg)

![](_page_37_Picture_0.jpeg)

#### Computer Room Analysis

![](_page_37_Picture_2.jpeg)

![](_page_37_Picture_3.jpeg)

![](_page_37_Figure_4.jpeg)

![](_page_37_Picture_5.jpeg)

Object parameter	Value
Emissivity	0.94
Object distance	6.6 ft
Ambient temperature	68.0°F
Label	Value
IR : max	90.5°F
IR : min	64.9°F
SP01	72.3°F
AR01 : max	90.5°F
AR01 : min	66.0°F
AR01 : max-min	24.6°F
AR01 : avg	74.5°F

IR Text Comment	Value
Section	Room
Equipment	
Additional information	
Fault	ProcessSCAN
Recommendation	No action Infrared Thermographic Services

![](_page_38_Picture_0.jpeg)

![](_page_39_Picture_0.jpeg)

![](_page_40_Picture_0.jpeg)

Elbow Complex with 2 degree lens 4X

Sile and a

Spot 1

108.8

### Spot 3 92.0

![](_page_40_Picture_3.jpeg)

F Spot 2

94.7

Damage to Elbow Complex found on IR Survey TV-& FM ansmission Towers

ProcessSCAN

Sand State

![](_page_42_Picture_0.jpeg)

![](_page_42_Picture_1.jpeg)

TV & FM Transmission Towers

![](_page_42_Picture_3.jpeg)

**Klyston** 

![](_page_42_Picture_5.jpeg)

# Bar Code Sorters

ElectroCom Automation L.P. DBCS IV MODE

![](_page_44_Picture_0.jpeg)

The mail is ~10F degrees cooler. This has a cooling effect on the belts/bearings, etc.

![](_page_44_Picture_2.jpeg)

Bar Code Sorters

![](_page_44_Picture_4.jpeg)

#### A low quality repair of a through-crack

### Degradation of thermal insulation

![](_page_45_Picture_3.jpeg)

![](_page_45_Picture_4.jpeg)

![](_page_45_Picture_5.jpeg)

![](_page_46_Figure_1.jpeg)

ProcessSCAN

Assume that we measure the temperature gradients  $\Delta T$  on a smokestack outer surface and determine the corresponding variations in thermal resistance  $\Delta R_t$ 

$$\Delta R_t = \frac{\left(1 + \frac{h_{out}}{h_{in}} + h_{out} R_t\right)^2}{h_{out} \left(T_{out}^a - T_{in}^a\right)} \Delta T_{out}^w$$

**Conclusion.** The typical IR camera temperature resolution of 0.1°C is equivalent to  $\Delta R_t = 0.032 \text{ m}^2 \text{KW}^{-1}$  (to compare to the total value  $R_t = 1.37 \text{ m}^2 \text{KW}^{-1}$ ) that is much better than in the case of absolute measurement.

**Example.** A smokestack is made of two brick layers separated with an air gap  $(R_t=1.37 \text{ m}^2\text{KW}^{-1})$ . The  $\Delta T=1.8^{\circ}\text{C}$  surface temperature signal is equivalent to  $\Delta R_t=0.33 \text{ m}^2\text{KW}^{-1}$  that can be explained by the destruction of the internal brick layer and the gas infiltration into the air gap.

![](_page_47_Picture_5.jpeg)

![](_page_47_Picture_6.jpeg)

![](_page_48_Figure_1.jpeg)

![](_page_48_Picture_2.jpeg)

![](_page_49_Figure_1.jpeg)

![](_page_49_Picture_2.jpeg)

![](_page_50_Figure_1.jpeg)

![](_page_51_Figure_1.jpeg)

Typical Smokestack Defects (Outline)

![](_page_51_Picture_3.jpeg)

![](_page_52_Figure_1.jpeg)

![](_page_53_Figure_1.jpeg)

SCHEMATIC PRESENTATION OF SMOKESTACKS

![](_page_53_Picture_3.jpeg)

![](_page_54_Figure_1.jpeg)

Evaluating absolute magnitudes of wall thermal resistance

$$T_{out}^{w} = \frac{T_{in}^{a} + \alpha_{out} T_{out}^{a} \left(\frac{1}{\alpha_{in}} + R_{t}\right)}{1 + \frac{\alpha_{out}}{\alpha_{in}} + \alpha_{out} R_{t}} \qquad R_{t} = \frac{T_{in}^{a} - \frac{\alpha_{out}}{\alpha_{in}} (T_{out}^{w} - T_{out}^{a}) - T_{out}^{w}}{\alpha_{out} (T_{out}^{w} - T_{out}^{a})}$$

Surface smokestack temperature variations vs. variations in experimental parameters

(central part of a typical smokestack involving brick refractory, mineral wool layer and reinforced concrete, smokestack wall thermal resistance  $R_t = 1.37 \ m^2 \ K W^{-1}$ , gas temperature inside is 125°C, ambient temperature is +18 °C, heat exchange coefficients:  $h_{in} = 23 \ W \ m^{-2} \ K^{-1}$ ,  $h_{out} = 16 \ W \ m^{-2} \ K^{-1}$ , smokestack outer surface temperature  $T_{out}^{W} = 22.53 \ ^oC$ )

Parameter variation $\Delta T_{in}^a = +1 \ ^oC$	Surface temperature variation, $\Delta T_{out}^{w}$ , ${}^{o}C$ 0.042	This is equivalent
$\Delta T^a_{out} = +1 \ ^oC$	0.96	to the total destruction
$\Delta h_{in} = \pm 1 \ W \ m^{-2} \ K^{-1}$	0.0058	of
$\Delta h_{out} = \pm 1 \ W \ m^{-2} \ K^{-1}$	-0.27	refractory

**Conclusion.** The error in measuring an absolute value of smokestack surface/ temperature is about  $\Delta T_{out}^{W}=1^{\circ}C$  that is equivalent to  $\Delta R_{t}=0.26 \text{ m}^{2}\text{KW}^{-1}$ (to compare to the total value  $R_{t}=1.37 \text{ m}^{2}\text{KW}^{-1}$ )

![](_page_54_Picture_8.jpeg)

Assume that we measure the temperature gradients  $\Delta T$  on a smokestack outer surface and determine the corresponding variations in thermal resistance  $\Delta R_t$ 

Evaluating variations in wall thermal resistance

$$\Delta R_t = \frac{\left(1 + \frac{h_{out}}{h_{in}} + h_{out} R_t\right)^2}{h_{out} (T_{out}^a - T_{in}^a)} \Delta T_{out}^w$$

**Conclusion.** The typical IR camera temperature resolution of 0.1°C is equivalent to  $\Delta R_t = 0.032 \text{ m}^2 \text{KW}^{-1}$  (to compare to the total value  $R_t = 1.37 \text{ m}^2 \text{KW}^{-1}$ ) that is much better than in the case of absolute measurement.

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![](_page_55_Picture_6.jpeg)

![](_page_55_Picture_7.jpeg)

![](_page_56_Figure_1.jpeg)

![](_page_56_Picture_2.jpeg)

![](_page_57_Figure_1.jpeg)

#### **Typical Smokestack Thermograms**

*Typically, a smokestack is surveyed from 6-7 ground observation points by collecting 40-60 thermograms in total.* 

![](_page_57_Picture_4.jpeg)

![](_page_58_Figure_1.jpeg)

**Typical Smokestack Thermograms** 

![](_page_58_Picture_3.jpeg)

![](_page_59_Figure_0.jpeg)

#### **Conclusions**

Warm areas observed on the smokestack surface, typically correspond to insulation deficiencies. The gravity of the defect can be reliably evaluated by solving the corresponding heat conduction problem. Surface temperature gradients can be used to estimate thermal resistance variations.

Cold areas of a particular pattern usually correspond to air in-leaks. A simple quantitative estimate allows to determine an air in-leak rate.

Aging smokestacks require the use of reliable diagnostic techniques. Infrared thermography is a fast and accurate method of condition monitoring.

Smokestack owners can use this form of condition monitoring to get accurate qualitative data to make decisions about repair activities.

From the practical point of view, any smokestack inspection should determine how long the smokestack can be used safely. To make that conclusion, an infrared survey should be complemented with a visual evaluation performed by an expert industrial chimney inspector.

![](_page_60_Picture_7.jpeg)